

Fast identification of mechanical and coupling parameters of porous materials by sensitivity analysis: application to conventional and auxetic foam

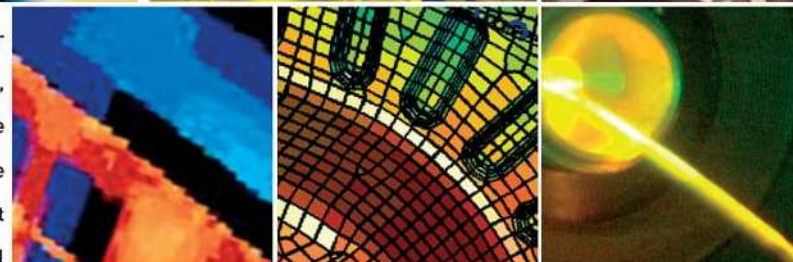
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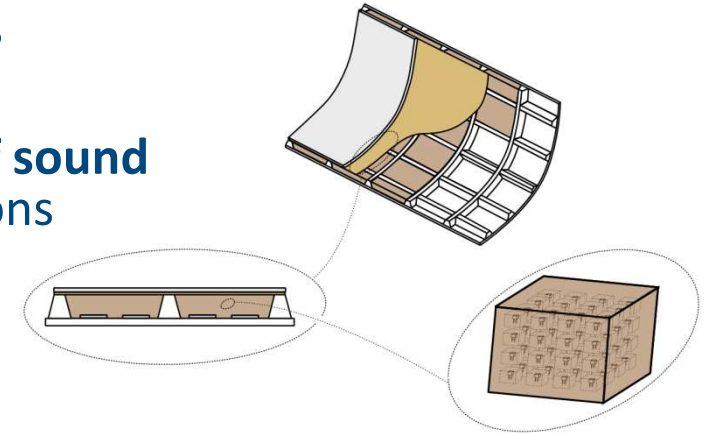
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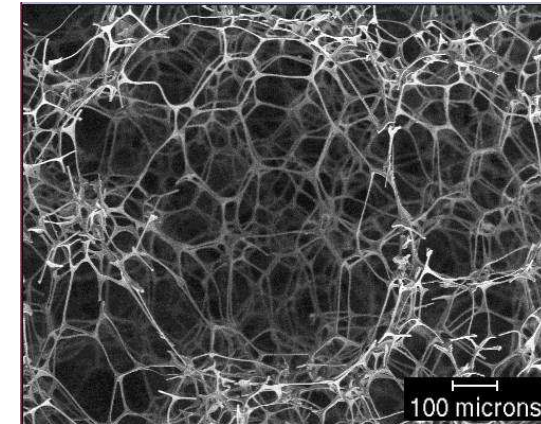
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- **Introduction**
- **Model description**
- **Sensitivity analysis**
- **Application on Melamine foam**
- **Application on PU-PE auxetic foam**
- **Conclusions**

- Use of porous materials for **smart vibroacoustics**
- Investigate new ways to **improve LF efficiency of sound packages**: use of passive resonant/active inclusions
- **Model-based** concepts
- Need for **fast, focused** identification procedures
- Case of **porous** materials : high number of parameters
 - Dedicated set-up for each parameter
 - Model updating from global information
- **Sensitivity** of parameters for **outputs of interest?**
- **Biot-Allard** model



- **Porous material: Two coupled phases (solid, fluid)**
- **Biot Theory:**
 - ‘Macroscopic scale’
 - Representative elementary volume
- **Homogeneous material**
- **Solid skeleton: Hooke’s law of linear-elasticity**
- **Pore space: saturated by the fluid phase**
- **Parameters (case of isotropic material): $E, \nu, \eta, \rho, \Phi, \sigma, \alpha_\infty, \Lambda, \Lambda'$**



gtmma.sourceforge.net/

Transversely isotropic materials:

$$\sigma_{xx}^s = (2G + A)e_{xx} + Ae_{yy} + Fe_{zz} - (1 - \phi)p$$

$$\sigma_{yy}^s = Ae_{xx} + (2G + A)e_{yy} + Fe_{zz} - (1 - \phi)p$$

$$\sigma_{zz}^s = Fe_{xx} + Fe_{yy} + Ce_{zz} - (1 - \phi)p$$

$$\sigma_{yz}^s = 2G'e_{yz}$$

$$\sigma_{xz}^s = 2G'e_{xz}$$

$$\sigma_{xy}^s = 2Ge_{xy}$$

where:

$$A = \frac{E(E'\nu + E\nu'^2)}{(1 + \nu)(E' - E'\nu - 2E\nu'^2)}$$

$$F = \frac{EE'\nu'}{E' - E'\nu - 2E\nu'^2}$$

$$C = \frac{E'^2(1 - \nu)}{E' - E'\nu - 2E\nu'^2}$$

$$G = \frac{E}{2(1 + \nu)}$$

For isotropic materials: $G = G'$, $F = A$, $C = A + 2G$

Parameters	Melamine (isotropic?)	Auxetic (transv. Isotropic?)
Mechanical	E, ν, η, ρ	$E, E', \nu, \nu', \eta, \rho$
Coupling	$\Phi, \sigma, \alpha_\infty, \Lambda, \Lambda'$	$\Phi, \sigma_x, \sigma_y, \alpha_{\infty x}, \alpha_{\infty y}, \Lambda_x, \Lambda_y, \Lambda'$

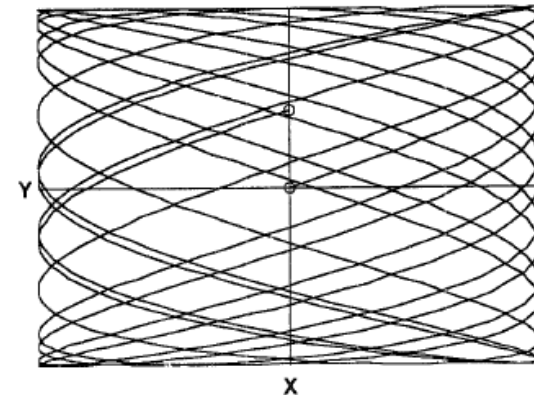
■ Sensitivity analysis

- **Inputs:** Foam parameters
- **Outputs** of interest: Z , α (frequency-dependent)
- **OAT sensitivity index** : finite differences
- Parameters **hierarchisation** and **screening**

$$s \approx \frac{f(x + \Delta x) - f(x)}{\Delta x}$$

■ FAST technique

- Based on **variance** analysis
- Estimation of **sensitivity indices**
 - First order / Total sensitivity index
 - $TSI(A) = SI(A) + SI(AB) + SI(AC) + SI(ABC)$
- (pseudo) **periodic sampling strategy** in the design space, **FFT** to estimate the SIs



Fourier-transform sensitivity analysis, G. Colonna, S. Longo, F. Esposito, M. Capitelli, Applied Physics B, 1994

Coupling parameters			
Parameters	Unit	Lower bounds	Upper bounds
Φ	[-]	0.98	0.99
σ	Nsm ⁻⁴	9000	11000
α_{∞}	[-]	1	1.03
Λ	[μ m]	80	100
Λ'	[μ m]	100	300
Mechanicals parameters			
Parameters	Unit	Lower bounds	Upper bounds
E	[kPa]	100	300
ν	[-]	0.14	0.45
ρ	Kgm ⁻³	8.5	14.5
η	[%]	5	15

Melamine sample 4,7 cm



Frequency range of interest

200-1600 Hz

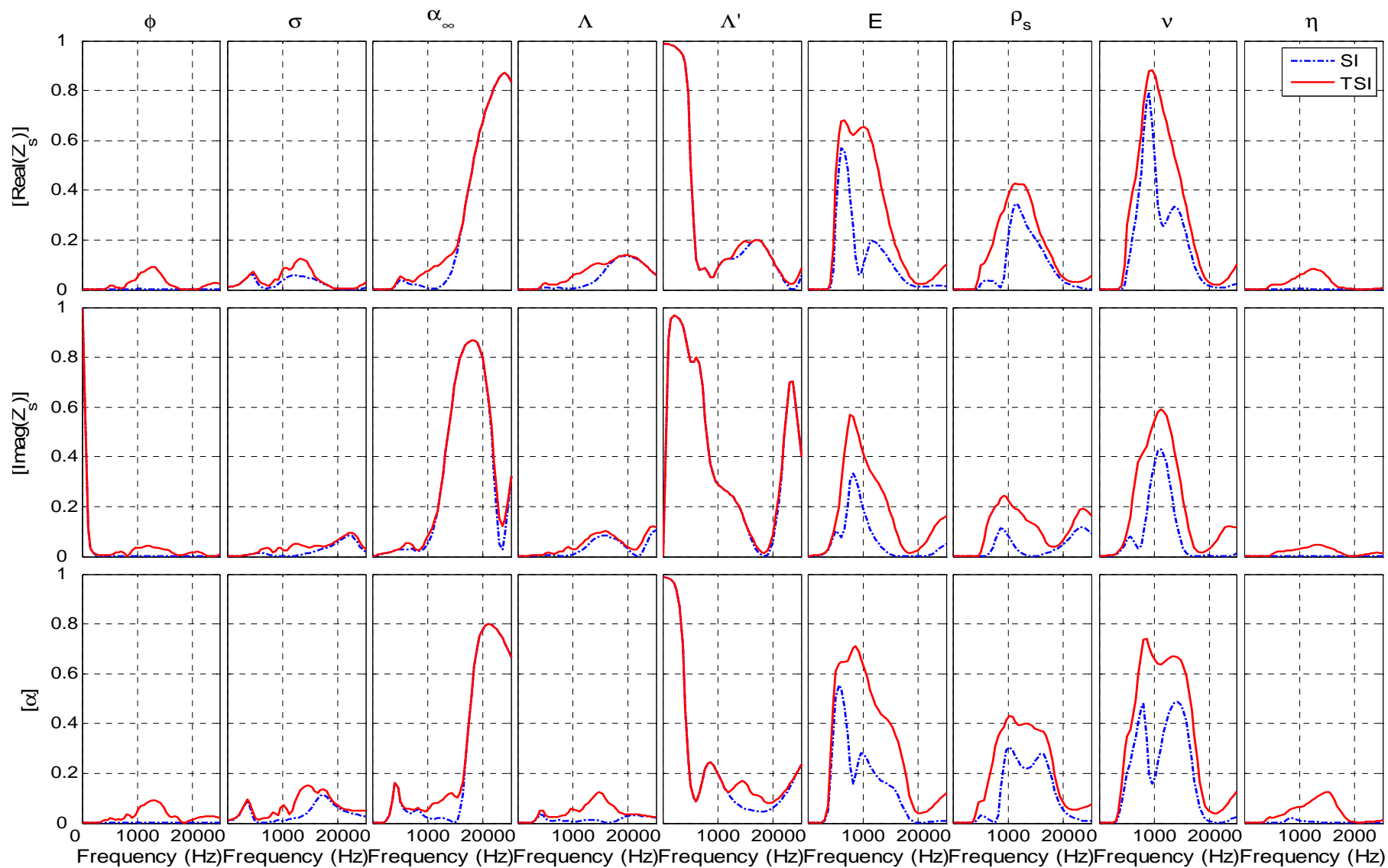
Outputs of interest

α, Z

(incident plane wave, sample backed by an impervious rigid wall)

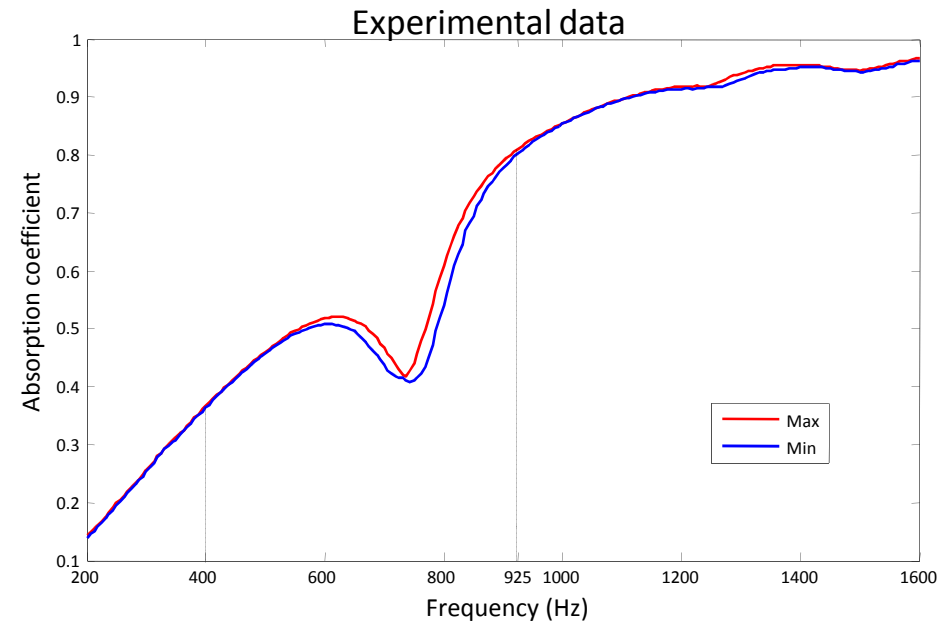
Small ranges, analytic formulation => fast convergence

NB Not always easy to obtain confident information about parameters ranges...



- Weighted Cost function for n tests on Nf frequency samples:

$$G = \sum_{i=1}^{Nf} w_i g(\omega_i)$$



$$g(\omega) = w_\alpha \left| \frac{\alpha(\omega) - \alpha_e(\omega)}{\alpha_e(\omega)} \right| + w_Z \left| \frac{|Z(\omega)| - |Z_e(\omega)|}{|Z_e(\omega)|} \right| \quad \alpha_e = \frac{1}{n} \sum_{i=1}^n \alpha_e^{(i)}$$

- **Simulation 1**

All parameters together

- **Simulation 2**

Most important parameters

Λ', ν, E, ρ

- **Simulation 3**

1°) Most important parameters

Λ', ν, E, ρ

2°) Second level parameters

$\alpha_\infty, \sigma, \Lambda$

- **Simulation 4**

1°) Most important parameters

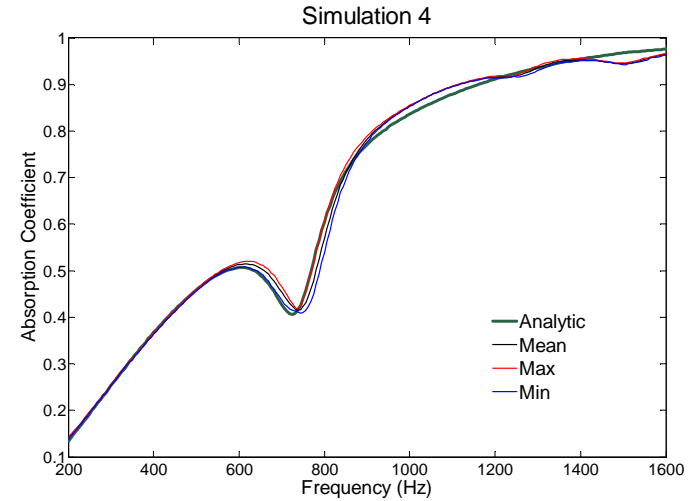
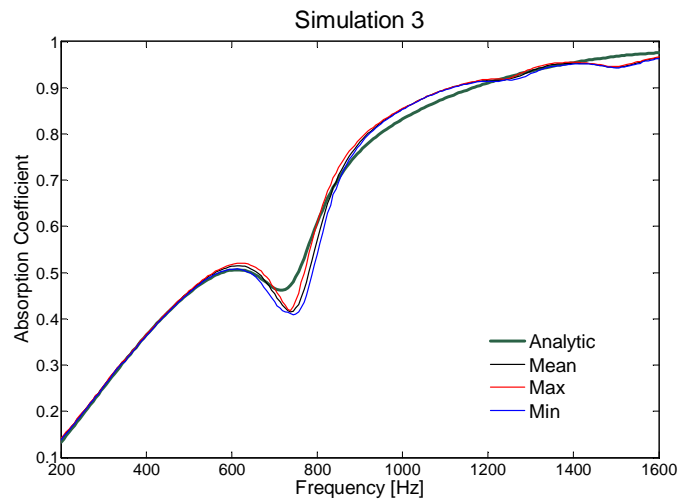
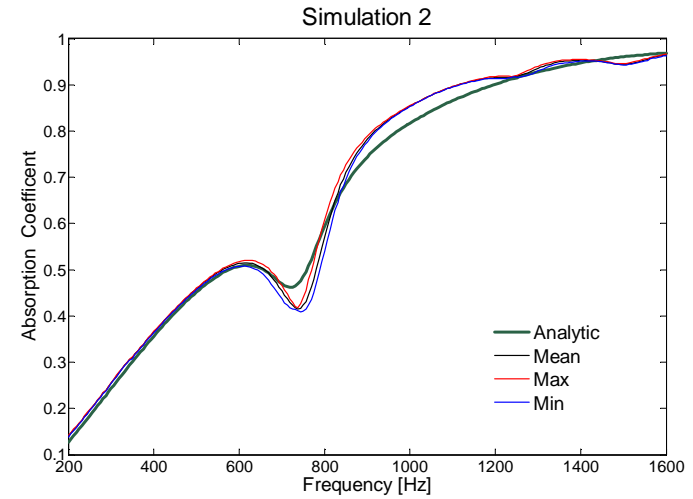
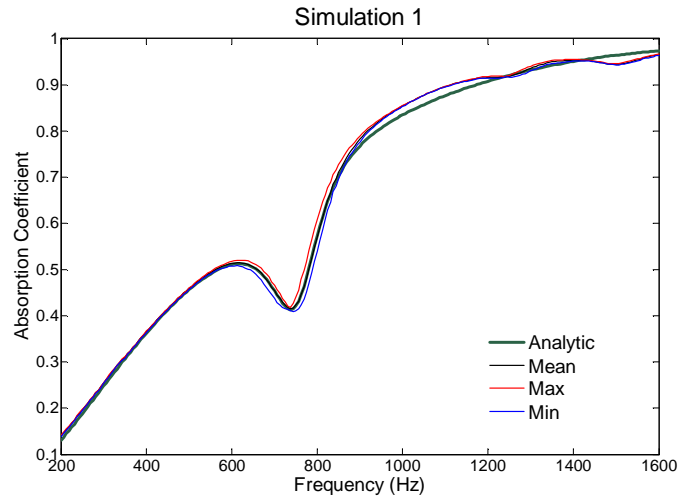
Λ', ν, E, ρ

2°) Second level parameters

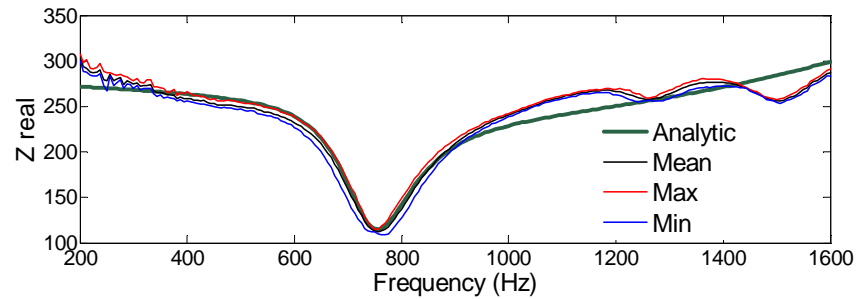
$\alpha_\infty, \sigma, \Lambda$

3°) Less important

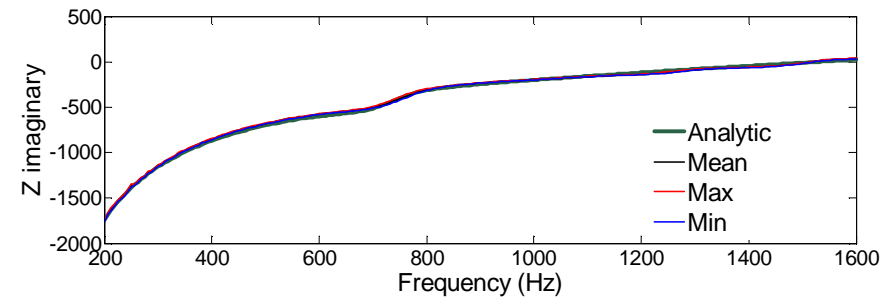
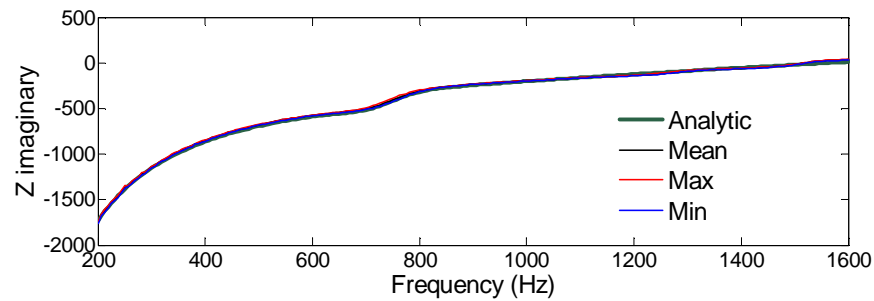
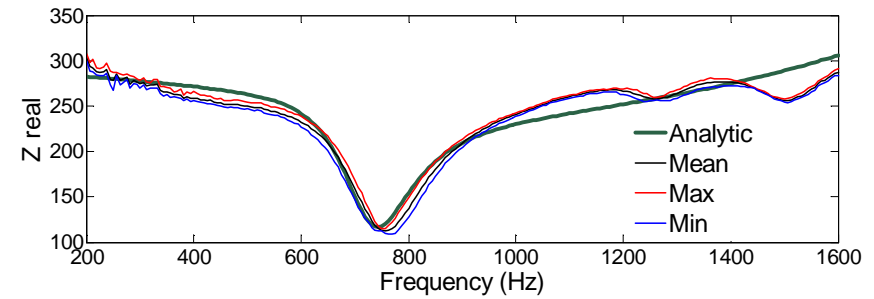
Φ, η



Simulation 1



Simulation 4



Parameters	Simulation			
	1	2	3	4
Λ' [μm]	168	177	177	177
E [kPa]	213	207	207	207
ν [-]	0.302	0.299	0.299	0.299
ρ [$\text{Kg}\cdot\text{m}^{-3}$]	14.5	14.5	14.5	14.5
α_{∞} [-]	1	1	1	1
σ [$\text{N}\cdot\text{m}\cdot\text{s}^{-4}$]	11000	10000	11000	11000
Λ [μm]	99.9	89.9	91.4	91.4
η [%]	0.138	0.100	0.100	0.056
Φ [-]	0.990	0.985	0.985	0.990
Cost function	14.6	24.7	18.5	16.3
Calculation time [s]	34.2	8.9	12.4	18.5

Classical PU-PE foam



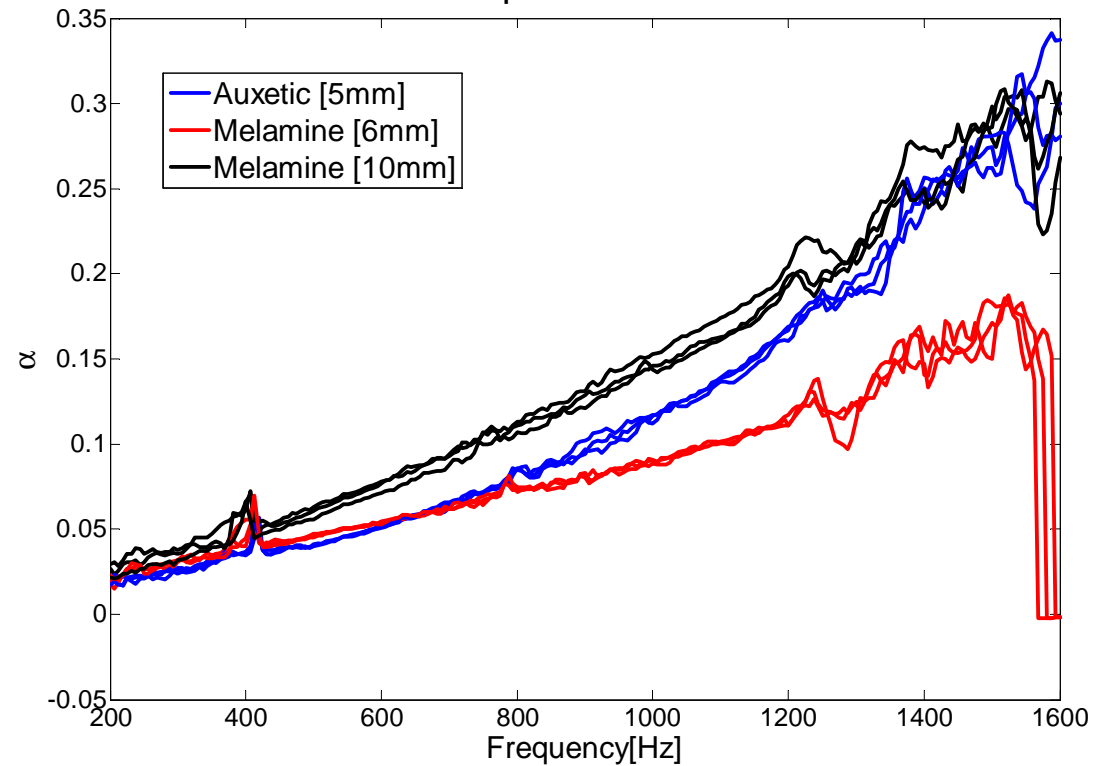
Specific process



Auxetic PU-PE foam



Absorption Coefficient



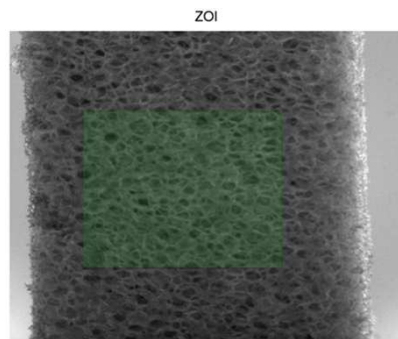
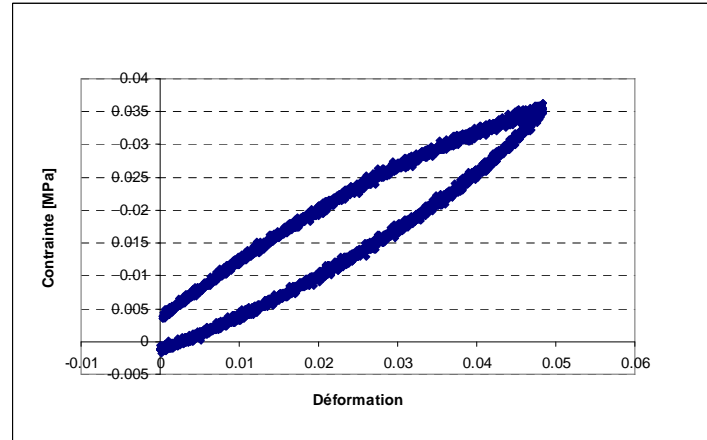
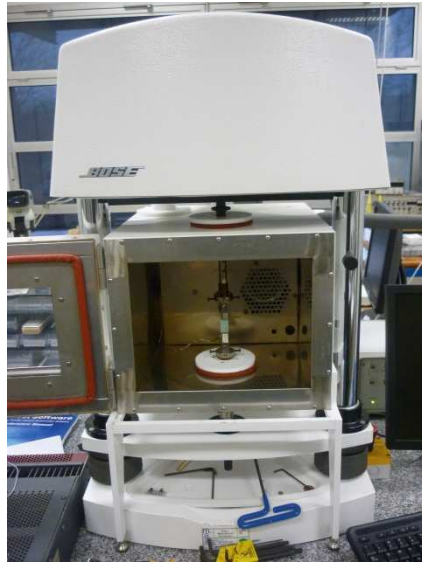
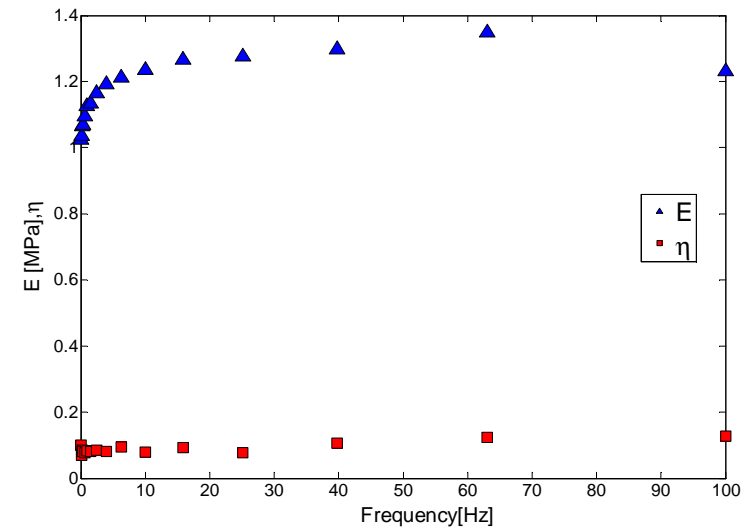


Image correlation

$$-0.82 < \nu < -0.1$$

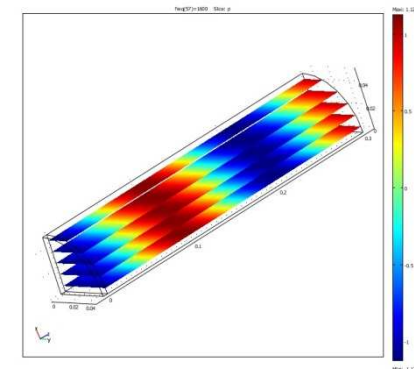


Coupling parameters			
Parameters	Unit	Lower bounds	Upper bounds
Φ	[-]	0.70	0.99
σ	Nsm ⁻⁴	1500	200000
α_{∞}	[-]	1	2
Λ	[μ m]	5	200
Λ'	[μ m]	5	400
Mechanicals parameters			
Parameters	Unit	Lower bounds	Upper bounds
E	[kPa]	1000	1400
E'	[kPa]	5	20
ν	[-]	0.25	0.35
ν'	[-]	-0.1	-0.82
ρ	Kgm ⁻³	20	34
η	[%]	0	25

Auxetic sample 5mm



FE analysis : more complex geometries & excitations, arbitrary constitutive law



**Large ranges, FE formulation
=> slow convergence (not yet!)**

- Identification of parameters for **global vibroacoustic indicators**
- Preliminary **parameters sensitivity analysis** to improve **efficiency** of model updating
- **Good results** for conventional melamine foam – all parameters required
- Case of **auxetic foams** :
 - **transversely isotropic** configuration
 - Interesting **acoustic properties**
 - work in progress: sensitivity analysis, parameters identification, correlation with DMA tests
- Next steps: use **validated model** for the design of the **smart foam**